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CO₂ Capture by PEI-Impregnated Alumina Sorbents

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Abstract: Direct air capture (DAC) or direct CO₂ extraction from ambient air is a promising approach to reduce greenhouse gas emissions caused by both distributed (location independent) and point sources (location specific). Solid sorbents have been considered as more effective for DAC compared to the liquid counterpart since they have a faster kinetic and avoid volatile and heat losses due to the absence of evaporation of liquids. In this study, the alumina - supported polyethyleneimine (PEI) material was chosen as solid sorbents and their CO₂ capture performance for different PEI loadings (20, 35, 50 wt%), flow rate (15, 30, 45 L/h) and adsorption temperatures (30, 40, 50, 60 °C) was investigated. Sorbents were prepared by using wetness impregnation method and their physical and chemical properties were characterized by several techniques such as N₂ adsorption - desorption (surface area, pore size and volume), Scanning Electron Microscopy - SEM (surface morphology, surface chemical composition). The CO₂ capture performance of sorbents were analyzed under different CO₂ concentrations and the cyclic (adsorption - desorption) behavior of the sorbents were tested. The results show that alumina-supported PEI adsorbents are promising materials for CO₂ capture with high CO₂ adsorption capacity and stability.

Keywords: PEI, Adsorption, CO₂ Capture, DAC, Greenhouse Gas, Alumina

Introduction

Carbon capture and storage (CCS) is crucial in the fight against climate change, which poses an existential threat to our planet. Despite being on the global agenda for decades, progress has been slow, insufficient, and sporadic. Anthropogenic CO₂ emissions are caused by our reliance on fossil fuels, accounting for 68% (or 37.5 GtCO₂) of the total greenhouse gas emissions in 2018. Capturing CO₂ at this scale requires resources and technologies that are currently unavailable. CO₂ capture is an expensive, energy-intensive process that is complicated by diverse emission sources varying in volume, composition, location, type, and industry or sector. However, the diversity of sources highlights the need for a multi-prong strategy that emphasizes the development of a wide range of CCS technologies, materials, and processes tailored to different sources (Gür, 2022).

Direct air capture (DAC) is a method of removing CO₂ directly from the atmosphere to achieve negative emissions. Despite concerns regarding its feasibility, there has been growing interest in exploring this technology as a climate change mitigation strategy. Proponents argue that even if carbon emissions were to stop

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completely, atmospheric CO₂ concentrations must be reduced expeditiously to mitigate the risks of climate change. DAC has the advantage of being able to capture CO₂ emissions from distributed sources, which make up almost half of global CO₂ emissions, unlike other technologies that mostly capture emissions from point sources (Yu et al., 2012).

Various DAC technologies exist including physical absorption, chemical absorption, adsorption, and membrane technologies, but none of them are yet matured for post-combustion power plants due to significant mass transfer limitations and the need to treat a huge amount of flue gas. Among these technologies, chemical absorption using aqueous alkanolamine solutions is proposed to be the most applicable technology for CO₂ capture before 2030, but it has drawbacks such as high equipment corrosion rate, high energy consumption in regeneration, and a large absorber volume required. Solid adsorption processes, such as impregnation or grafting of amines, have been suggested to overcome these problems. Chemical modification of solid materials with high surface area is a key area of research to improve CO₂ adsorption and selectivity for DAC. The use of organic groups such as amines and inorganic metal oxides like alkali or alkali-earth metals has garnered particular interest due to their basic properties. Covalent bonding between the acidic CO₂ molecules and modified basic active sites on the surface enhances CO₂ adsorption. Although amine-based adsorbents have a low heat of regeneration compared to aqueous amines due to the low heat capacity of solid supports, their low CO₂ adsorption capacity and high cost hinder commercialization. To improve amine-based adsorbents, recent approaches include using amine with high nitrogen content, preparing supports with high amine loading, and effective methods for amine introduction. Amine-based adsorbents can be categorized as amine-impregnated and amine-grafted materials based on their interaction with the supports. Typically, amine-grafted adsorbents exhibit higher adsorption rates and stability in cyclic runs than amine-impregnated ones. However, the grafted amount of amine depends on surface silanol groups, which can result in lower amine loading compared to impregnation. Although higher amine loadings can be achieved through impregnation, it can lead to a large diffusion resistance. The feasibility of operating under practical conditions, containing 3-5% water and 10-15% CO₂ at 55°C in coal power plant flue gases, requires evaluating kinetics and heat effects (Yu et al., 2012).

There are several types of amines that are commonly used for solid adsorbents for CO₂ capture. Primary amines such as monoethanolamine (MEA), diethanolamine (DEA) and triethylenetetramine (TETA) contain one amino (-NH₂) group and they are well known their high CO₂ affinity whereas secondary amines like piperazine and N-methyldiethanolamine (MDEA) have two amine groups and they have a lower CO₂ affinity compared to primary amines. N, N-dimethylethanolamine (DMEA) and N, N-dimethylcyclohexylamine (DMCHA) are known as tertiary amines that have three amino groups and have the lowest CO₂ affinity in this class. When polymers are functionalized with amine groups which are called as amine-functionalized polymers, their CO₂ adsorption capacity can be increased due to their high surface area (Wang et al., 2015). Polyethyleneimine (PEI) and polyvinylamine (PVAm) are the most known examples of this class. Primary amines and tertiary amines are often used in post-combustion and pre-combustion CO₂ capture, respectively. Amine-functionalized polymers are used in both post- and pre-combustion CO₂ capture processes.

PEI is a high molecular weight polymer with a branched structure and abundant amino groups that allow for strong CO₂ adsorption. The high molecular weight and branched structure provide a large number of amine groups, which increases the CO₂ adsorption capacity of the material. In addition, PEI is known to have excellent stability and resistance to degradation under harsh conditions such as high temperatures and acidic environments, which are commonly encountered in CO₂ capture processes (Li et al., 2021). This stability ensures the material can be used repeatedly without significant loss of CO₂ adsorption capacity. PEI also has low volatility, which means that it does not evaporate or escape easily into the gas stream during CO₂ capture, reducing the possibility of amine emissions and environmental pollution. This low volatility is attributed to the high molecular weight of the polymer and the strong interactions between the amine groups and the support material.

Xu and his colleagues have investigated the impact of several factors on the capacity of polyethyleneimine (PEI) for adsorbing carbon dioxide (CO₂) (Xu et al., 2002a). These factors include PEI loading, gas conditions, temperature, moisture, and the type of support used. Results have shown that a higher PEI loading led to a significant increase in CO₂ adsorption capacity, although this was accompanied by a reduction in surface area, pore size, and pore volume. The highest CO₂ adsorption capacity was observed with 75 wt.% PEI loading in PEI-impregnated MCM-41 under pure CO₂ at 75°C. However, the highest amine efficiency was found with 50 wt% PEI loading and decreased with increasing PEI loading. This suggests that amine loading is not directly related to CO₂ adsorption since the formation of aggregated amine on supports can reduce the amine accessible to CO₂. Temperature was also found to affect CO₂ adsorption capacity, with lower temperatures resulting in decreased capacity due to the exothermic nature of CO₂ adsorption. However, at low temperatures, bulk-like

PEI formation inside pores could lead to diffusion-limited CO₂ adsorption. Higher temperatures were associated with higher CO₂ adsorption capacity, likely due to the increased diffusion rate of CO₂ into bulk-like PEI and the faster reaction rate of CO₂ with PEI. Moisture was found to have a positive effect on CO₂ adsorption capacity when present at concentrations lower than that of CO₂ with carbamate and bicarbonate formation under anhydrous and hydrous conditions respectively.

Flow rate is also important parameter that affects the contact time between the CO₂ and the adsorbent, and a higher flow rate typically leads to a shorter contact time. As a result, the CO₂ may not have enough time to adsorb onto the solid adsorbent and the overall capture efficiency may be reduced. On the other hand, a lower flow rate can increase the contact time between the CO₂ and the adsorbent leading to higher capture efficiency. However, a very low flow rate may also lead to a reduced efficiency due to mass transfer limitations. Shafeeyan et al. (Shafeeyan et al., 2015) studied the adsorption of CO₂ onto ammonia-modified activated carbon and measured the breakthrough adsorption of CO₂ on fixed beds of commercial granular activated carbon (GAC) and ammonia-modified GAC (OXA-GAC) adsorbents. They measured the breakthrough curves from dynamic column measurements at temperatures ranging from 30 to 60 °C with a feed gas flow rate that varied from 50 to 100 mL.min⁻¹ and a total pressure of 1.0 atm. They found that the breakthrough time of CO₂ adsorption decreased with increasing flow rate indicating that the flow rate has a significant effect on the CO₂ adsorption capacity of the adsorbent. A study by Darunte et al. investigated the effect of flow rate on CO₂ adsorption by a novel amine-functionalized metal-organic framework (MOF), MIL-101(Cr)-NH₂. They found that the CO₂ adsorption capacity of MIL-101(Cr)-NH₂ increased with increasing flow rate and the maximum CO₂ adsorption capacity was achieved at a flow rate of 100 mL/min (Darunte et al., 2016). However, Goepfert and his colleagues found that total CO₂ adsorption capacity of the silica supported PEI adsorbents did not show the high dependency on the flow rate (Goepfert et al., 2014). When they increase the flow rate from 335 to 945 mL min⁻¹, this resulted with decrease in the total adsorption capacity from 50 to 47 mg CO₂ g⁻¹ when 33% PEI by weight was used and increase in PEI loading caused to increase in effect of flow rate on the CO₂ adsorption capacity.

Adsorption temperature is another important factor that can affect the CO₂ capture efficiency. At low temperatures, the adsorption of CO₂ onto the adsorbent surface is generally more favorable because the kinetic energy of the CO₂ molecules is lower, which makes them more likely to adsorb onto the surface. This can lead to a higher CO₂ capture capacity at lower temperatures. However, it's worth noting that the rate of adsorption may be slower at low temperatures, which can reduce the overall capture efficiency. At high temperatures, the adsorption of CO₂ onto the adsorbent surface is generally less favorable because the kinetic energy of the CO₂ molecules is higher, which makes them less likely to adsorb onto the surface. As a result, the CO₂ capture capacity may be reduced at higher temperatures. However, high temperatures can also result in desorption of previously adsorbed CO₂, which can be beneficial for the regeneration of the adsorbent and the reusability of the system. Goepfert et al., found that increase in temperature results with the decrease in total CO₂ adsorption from air by silica-supported PEI adsorbents with loading of 33% and 50% by weight (Goepfert et al., 2014). However, increase in temperature from 25 to 35 °C slightly increased the total adsorption from air and significantly decreased when the temperature increased up to 85 °C when air under 10 ppm was used.

The support material used in direct air capture (DAC) with polyethyleneimine (PEI) sorbents plays a critical role in determining the overall performance of the system. The support material serves as a substrate for the PEI sorbent, providing a large surface area for CO₂ adsorption and facilitating mass transfer between the gas and solid phases. Different support materials can vary in their pore structure, surface chemistry, and other properties that can impact the adsorption capacity, selectivity, and stability of the sorbent. Solid amine sorbents are commonly supported by silica, but alumina and titania could be better options as they can address some of silica's limitations. Silica, for instance, experiences a structural change and loses its CO₂ capture capability when exposed to steam. While PEI-impregnated sorbents can be regenerated through various methods, including temperature-vacuum alternation, hot CO₂ flow, and water vapor, a urea-forming reaction can lead to irreversible PEI decomposition when CO₂ reacts with two amine groups at or above 135 °C in dry conditions. Water vapor regeneration can prevent this decomposition to some extent, but it cannot eliminate urea formation. Steam regeneration or steam-stripping is a convenient method for thermal regeneration, especially in industrial processes where waste steam is typically around the temperature required for water vapor regeneration. Nevertheless, porous silica such as MCM41, SBA-15, and MCF may not be stable in water vapor, leading to a loss of CO₂ uptake capacity (Xu et al., 2002b). Alumina supports, however, are more resistant to structural changes and degradation during regeneration with water vapor due to their crystallinity and lower hydrophilicity.

The CO₂ capture performance of PEI-loaded alumina sorbents have been addressed several times in the literature. Goepfert and colleagues described the preparation of an alumina-supported PEI sorbent for DAC

(Goeppert et al., 2011). The sorbent was prepared by impregnating gamma-alumina with a solution of PEI, followed by drying and calcination. The resulting sorbent had a CO₂ adsorption capacity of 73 to 75 mg CO₂/g adsorbent (1.65 to 1.71 mmol/g). However, when they use alpha-alumina supported PEI rather than gamma-alumina supported PEI, the resulting sorbent had a CO₂ adsorption capacity of 1.02 mmol/g at 25 °C and atmospheric pressure and 1.41 mmol/g at 50 °C and atmospheric pressure. All of these studies have been carried out using methanol as a solvent, however, when the resulting supported-PEI were treated with a mixture of acetic acid and acetic anhydride, CO₂ adsorption capacity of the resulting sorbent reached the 1.85 mmol/g (Gargiulo et al., 2007) and Zhang et al. (Zhang et al., 2013) reported that the adsorbent exhibited a high CO₂ adsorption capacity of 2.5 mmol/g for alumina sorbents with PEI loading of 30 wt% and 40 wt%, respectively. Lin et al. (Lin et al., 2013) reported that at 100 wt% PEI loading, the CO₂ adsorption capacity at 0.15 bar reached a very competitive value of 4.2 mmol g⁻¹ at 25°C and 3.4 mmol g⁻¹ at 50°C, while Chen et al. (Chen et al., 2014) found that the optimal PEI loading was 50 wt% and the adsorbed amount of CO₂ was 2.5 mmol g⁻¹ at 25 °C and 1 bar. The literature studies summarized above for the CO₂ capture from ambient air (400-450 ppm CO₂) on PEI-loaded alumina sorbents indicate that CO₂ adsorption capacity of sorbents varies between 1.65-4.2 mmol/g suggesting that PEI-loaded alumina has an important potential as CO₂ sorbent material. However, the significant difference in the CO₂ adsorption capacity and the optimum PEI loading shows that the relation between the CO₂ capture performance of the material and their physical and chemical properties needs to be further addressed to develop high-performance sorbents. In addition, the CO₂ capture performance of the related material at higher CO₂ pressure is lacking in the literature. This needs to be investigated to understand the effect of CO₂ concentration on the CO₂ adsorption capacity of the sorbents, which is especially important to determine the performance of sorbents for the CO₂ capture by pressure-swing adsorption (PSA) process.

To address the related issues, the CO₂ capture by the alumina-supported PEI adsorbents with different PEI loadings have been investigated at different CO₂ concentrations (e.g., 1 and 17%), flow rates and adsorption temperatures. Sorbents were prepared by the impregnation method and characterized by several techniques to link sorbent properties with CO₂ capture performance.

Method

Preparation of Adsorbents

PEI-loaded alumina sorbents were prepared by the impregnation method. F-200 activated gamma alumina adsorbent was purchased from BASF. The sorbent preparation process involves several steps. First, alumina pellets were washed with methanol and dried overnight in an oven at 100 °C. Then, the clean alumina spheres were mixed with 20 ml of methanol and kept under stirring for one hour. Next, 20 ml of methanol was mixed with a specific amount of PEI depending on the desired PEI loading and the resulting mixture was stirred for one hour. The PEI-methanol solution was then added dropwise to alumina pellets suspended in 20 mL of methanol and stirred for another hour. The resulting impregnated alumina pellets were then dried using a rotary evaporator at 50 °C under vacuum with a rotation of 100 rpm and a pressure of 100 mbar. The pellets were subsequently dried in a vacuum oven at 60 °C overnight. Finally, the pellets were weighed, and the PEI loading was calculated and recorded. The PEI loadings were 20%, 35% and 50% by weight and 2 g pellets were prepared for each batch.

CO₂ Adsorption and Desorption Experiments

The CO₂ adsorption and desorption studies were performed at two different CO₂ concentrations by using two different experimental setups. The experiments with a CO₂ concentration of 1% were conducted using Micromeritics' AutoChem II 2920 Chemisorption Analyzer equipped with a TCD detector with a U-tube sorbent bed. The sorbents were loaded to the reactor and heated to 110 °C under N₂ atmosphere for 2 hours to remove water and volatile components. The sorbents were then cooled to the adsorption temperature (40, 50, or 60 °C) The adsorption experiments were carried out at 40 °C under 1% CO₂/N₂ atmosphere with a flow rate of 25 ml/min for 1 hour for desorption, at the end of the adsorption period, the gas was switched from CO₂/N₂ to N₂ (inert gas) and left for 0.5 hours with a flow rate of 50 ml/min. Under the inert gas atmosphere, the temperature was increased to 120 °C with a flow rate of 50 ml/min and a heating rate of 5 °C/min and left for 1 hour. The sample was then cooled down to 40 °C under N₂ flow with 50 ml/min flow rate and the experiment was finalized.

The adsorption-desorption experiments with a CO₂ concentration of 17% were performed in a home-built setup containing a quartz reactor (ID: 10 mm), a tubular oven, flow control units and a CO₂ detector. Sorbents were loaded into the reactor and heated to 110 °C under N₂ atmosphere with a flow rate of 20 L/h. The sample was kept at that temperature for 1 hour to remove water and volatile components. The sample was then cooled to the desired adsorption temperature (40, 50, 60 °C) and the gas flow was switched from N₂ to a 17% CO₂ - N₂ gas mixture. Adsorption experiments were carried out under a 17% CO₂-N₂ gas mixture atmosphere with a flow rate of 15 – 30 – 45 L/h CO₂-N₂ for 1 hour. At the end of the adsorption period, the gas was switched from CO₂-N₂ to N₂, and the system was left for 1 hour with a flow rate of 20 L/h. Under an inert gas atmosphere, the temperature was increased to 120 °C with a flow rate of 20 L/h and a heating rate of 5 °C/min and the system was left for 1 hour. The system was finally cooled down to 40 °C under an N₂ flow with a flow rate of 20 L/h.

Sorbent Characterization

The amine loading of sorbents was determined by elemental analysis. The Leco Truspec CHN-2007S was utilized and the nitrogen content of sorbents was used to quantify the amine loading. The surface area, pore volume and pore size distribution of sorbents were analyzed by N₂ adsorption-desorption using Micromeritics Tristar II. The surface area of sorbents was determined using the Brunauer – Emmett – Teller (BET) method, while the pore volume and pore size distribution were calculated using the Barrett–Joyner–Halenda (BJH) method. Prior to analysis, alumina-supported PEI adsorbents were degassed at 110 °C for 2 hours, while alumina spheres were degassed at 60 °C for 12 hours. Thermal gravimetric analysis (TGA) was conducted to determine the desorption and decomposition temperature of CO₂, H₂O, and PEI under N₂ environment by using Perkin Elmer Diomand TG/DTA analyzer. The analysis was carried out at 25-900 °C with a heating rate of 10 °C/min and for 2 hours. SEM-EDX analysis was carried out to investigate surface morphology by using FEI QUANTA 250 FEG analyzer.

Results and Discussion

TGA analysis was performed to determine the thermal stability and decomposition behavior of the adsorbent. One of the challenges in direct air capture is the regeneration of the adsorbent after it is saturated with CO₂. Regeneration typically involves heating the adsorbent to high temperatures (70-100 °C), but the excessive heating can cause thermal degradation of the adsorbent, leading to a decrease in its performance over time. To prevent thermal degradation of the sorbent and to determine the safe regeneration window, TGA analysis was applied.

Figure 1 shows TGA curve of 50% PEI containing alumina between 25 °C and 800 °C. As seen from the Figure, the first weight loss occurs between 25 and 1500 °C, which is related to water and CO₂ removal. This is followed by a stepwise weight loss between 150 and 600°C, which is attributed to the removal of volatiles caused by PEI degradation via the breaking of the polymer chains. This finding suggests that the regeneration temperature needs to be less than 150°C since above 150°C PEI on gamma-alumina starts to degrade. The PEI-related weight loss is around 30%, which is less than the expected weight loss (33.3%) based on PEI loading. Since there is no clear division between weight loss related to water and CO₂ removal and PEI degradation, it is difficult to determine PEI loading by TGA analysis. Therefore, CHNS analysis was applied to determine the PEI loading of sorbents by the nitrogen contents of sorbents. The PEI loadings determined by CHNS analysis are shown in Table 1. As seen from the Table, the actual PEI loadings of sorbents are 19.6, 27.5 and 27.4 wt% for 20PEI, 35PEI and 50PEI, respectively. The PEI loadings for 35PEI and 50PEI are almost the same suggesting that PEI does not dissolve in methanol completely for PEI loading greater than 30% in the specified PEI/methanol ratio.

It is well known that amine loading directly affects textural properties of sorbents such as surface area, pore volume and size. The extent of this effect for different PEI loading was analyzed by N₂ adsorption-desorption experiments. Results are shown in Table 2 indicating that the surface area and pore volume of sorbents decreases significantly with PEI loading due to the pore-filling effect of the polymer. The degree of reduction is much higher compared to PEI-loaded sorbents with similar PEI loadings. This is related to the poor solubility of PEI in methanol in the specified impregnation conditions. This was also proved by SEM-EDX analysis. SEM-EDX analysis was performed on both alumina and PEI-loaded alumina sorbents to study the morphology and elemental composition of the adsorbent material.

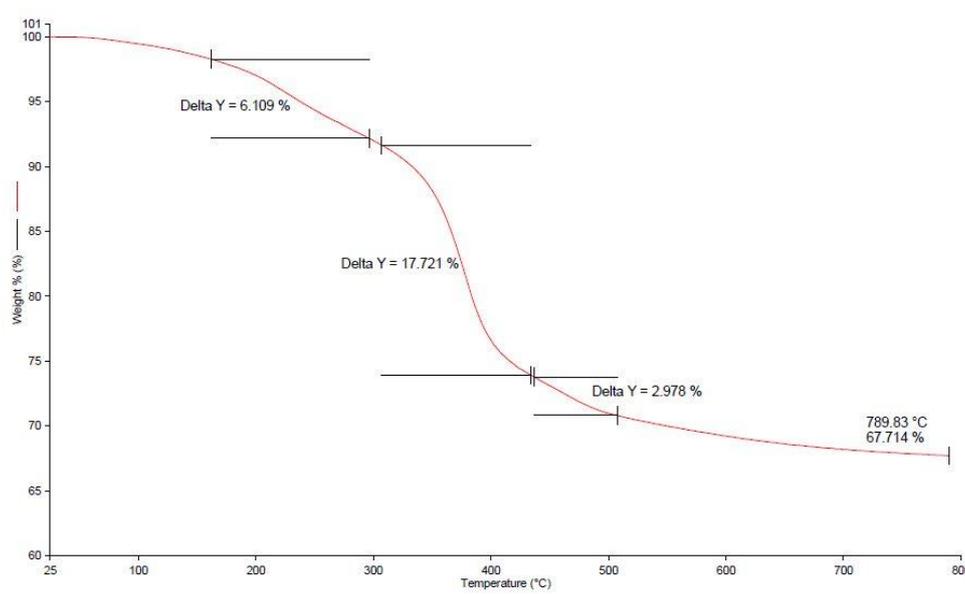


Figure 1. TGA Analysis of PEIM_50 Adsorbent

Figure 2 shows SEM images and elemental map of sorbents. Results show that C, O and N have more uniform distribution on alumina-supported PEI with a loading of 50% by weight contrary to loadings of 20% and 35% (**Figure 2**). However, for all PEI-containing sorbents PEI loading concentrates to specific sites of the support indicating uneven distribution of PEI on the surface. This can be attributed to the poor solubility of PEI in methanol or insufficient mixing process, which supports the findings of N₂ adsorption-desorption analysis. Surface composition of carbon and nitrogen was also determined from EDX analysis and listed in **Table 2** in comparison the bulk composition of the related elements. As seen from the Table, surface compositions of carbon and nitrogen are almost doubled compared to bulk composition. This is expected considering that PEI molecules cover surface sites.

Table 1. BET Analysis result of adsorbents

Adsorbents	BET Surface Area (m ² /g)	Volume of Pores (cm ³ /g)
Pure Al ₂ O ₃	327.5273	0.291974
PEIM_20	43.2688	0.088509
PEIM_35	21.7087	0.042147
PEIM_50	8.44300	0.013505

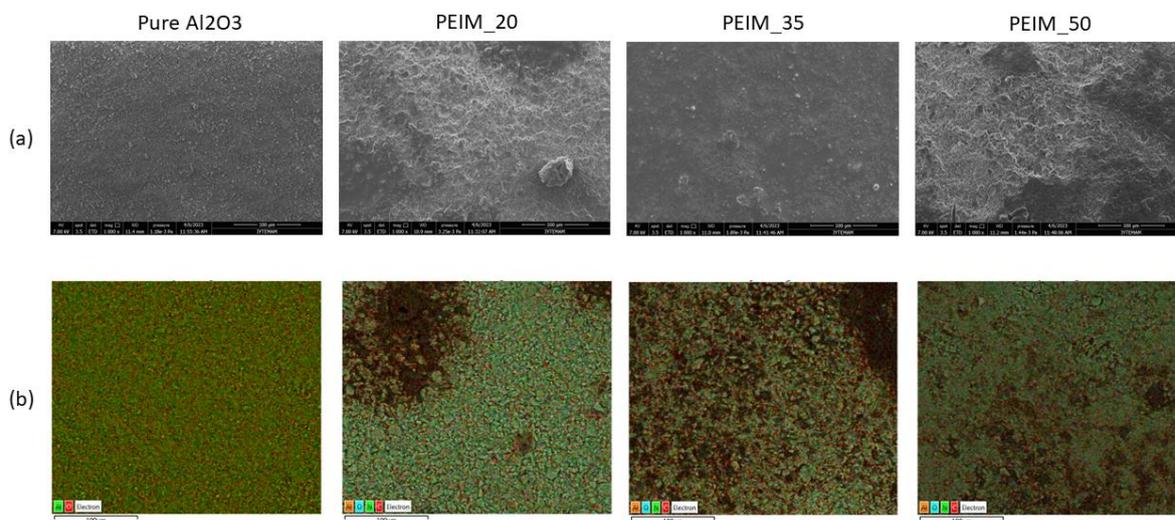


Figure 2. SEM images of adsorbents, (a) Adsorbents surface (magnification: 1000x), (b) Adsorbents surface (EDX, magnification: 1000x)

Table 2. Elemental composition of adsorbents

Adsorbents	Theoretical	CHNS	SEM-EDX
PEIM_20 (wt%)			
C	9.29	13.41	26.76
H	1.96	3.81	NA
N	5.42	5.34	9.68
PEIM_35 (wt%)			
C	14.45	15.51	40.22
H	3.05	4.41	NA
N	8.43	7.03	16.16
PEIM_50 (wt%)			
C	18.57	15.68	44.16
H	3.92	3.94	NA
N	10.83	6.99	17.78

CO₂ adsorption capacity of sorbents were first tested under 1% CO₂ in chemisorption setup by a TCD detector. Since the TCD detector works based on the change in thermal conductivity, it is sensitive to all gases, which complicates obtaining CO₂ adsorption profiles. However, it can still be used to determine the CO₂ adsorption capacity of sorbents by using their desorption curves. By using this approach, CO₂ adsorption capacity of sorbents were calculated from desorption peak areas and listed in Table 3. As seen from the table, CO₂ adsorption capacities of PEIM_35, PEIM_50, alumina and PEIM_20 are 90.5, 63.1, 50.3 and 26.2 mg CO₂/g sorbent, respectively. Results show that alumina has a higher CO₂ capture capacity than the sorbent with 20% PEI loading. This can be ascribed to the significant reduction in surface area and pore volume of PEIM_20 compared to pure alumina, which leads to very few active sites for CO₂ adsorption. Even if the CO₂ adsorption on PEI is more chemically favored compared to the CO₂ adsorption on alumina, the dramatic decrease in surface area and pore volume of PEIM_20 results in lower CO₂ adsorption. A similar effect was not observed for PEIM_35 and PEIM_50, which show higher CO₂ adsorption compared to pure alumina. The enhancement of CO₂ adsorption by PEI for these sorbents are more dominant than the reduction of CO₂ adsorption due to the low surface area and pore volume. PEIM_35 shows higher CO₂ adsorption capability compared to PEIM_50, which can be explained by steric hindrance and a reduction in the accessibility of the amine groups to the CO₂ molecules at high PEI loading. Another possible explanation is that at higher PEI loadings, there may be an increase in the number of free amine groups that are not attached to the surface of the adsorbent. These free amine groups can interact with each other and form bulky PEI aggregates which can reduce the available surface area for CO₂ adsorption and lower the CO₂ adsorption capacity.

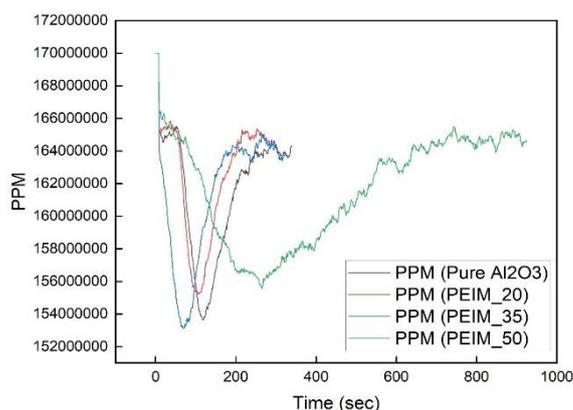


Figure 3. Adsorption of CO₂ by solid adsorbents under 17% CO₂ (ppm) atmosphere.

Table 3. CO₂ adsorption capacities of adsorbents for 1% and 17% CO₂

	Adsorbents	CO ₂ Adsorption Capacity (mg CO ₂ /g adsorbent)
1% CO ₂	PEIM_20	26.2
	PEIM_35	90.5
	PEIM_50	63.1
17% CO ₂	PEIM_20	6.25
	PEIM_35	6.69
	PEIM_50	24.0

CO₂ adsorption behaviors of sorbent were also studied under 17% CO₂ environment. Figure 3 shows CO₂ adsorption curves for all sorbents. Different from the results obtained at low CO₂ concentration, PEIM_50 exhibits the highest CO₂ adsorption capacity. CO₂ adsorption on the related sorbent occurs in a long adsorption period. The other sorbents behave differently, i.e., they show a fast CO₂ build-up (e.g., sharp decrease in CO₂ concentration) and short adsorption times. Among them, CO₂ adsorption capacity decreases in order by PEIM_35 > alumina > PEIM_20. The CO₂ adsorption capacity of sorbents were also calculated by using areas under the curve and tabulated in Table 3. Calculations indicate that PEIM_50 has almost 4 times higher adsorption capacity than PEIM35 and PEIM_20. The latter two show almost the same performance. The calculated adsorption capacities of sorbents are quite low compared to those obtained at low CO₂ concentrations. This is attributed to high internal mass transfer resistance of sorbents at high flow rate conditions. The gas flow rate for experiments conducted at high CO₂ concentrations is almost 10-fold higher than those performed at low CO₂ concentration. This suggests that the CO₂ adsorption on PEI-loaded sorbents is diffusion limited due to their relatively low pore size.

The effect of diffusion limitation of PEI-loaded sorbents was also evaluated by experiments conducted at different flow rates. Figure 4 shows CO₂ adsorption of the best performance sorbent (PEIM_50) at flow rates of 15, 30 and 45 L/h under 17% CO₂ atmosphere. The figure shows that increase in flow rate results with the decrease in CO₂ capture capacity (Figure 4 and Table 4) and there is a dramatic decrease in adsorption behavior and capacity (Table 4) between the flow rates of 15 and 30 L/h. This indicates that above the flow rate of 15L/h the gas flow rate is so fast that there is not enough time for adsorption due to relatively slow diffusion processes.

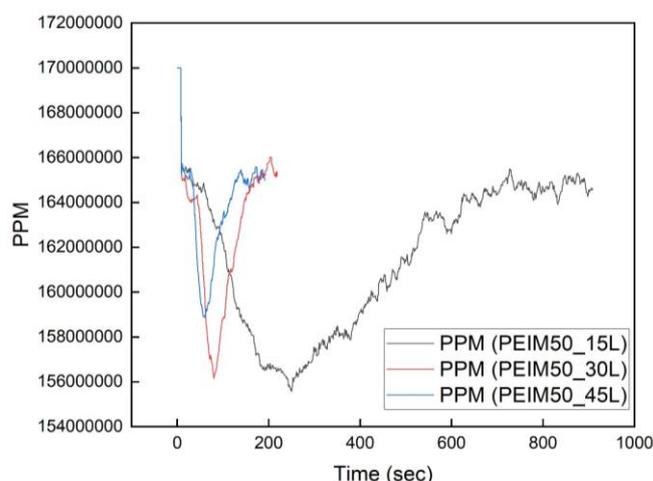


Figure 4. Effect of flow rate on the CO₂ adsorption via the alumina-supported PEI adsorbent with a loading of 50% by weight.

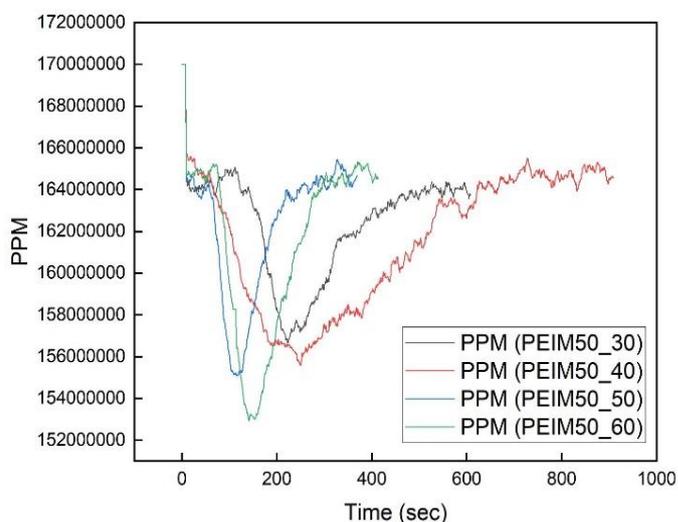


Figure 5. Effect of adsorption temperature on the CO₂ adsorption via the alumina-supported PEI adsorbent with a loading of 50% by weight.

Table 4. Effect of flow rate and adsorption temperature on CO₂ adsorption capacity of PEIM_50

	CO ₂ Adsorption Capacity (mg CO ₂ /g adsorbent)
Flow Rate (L/h)	
15	24.0
30	3.57
45	2.49
Adsorption Temperature (°C)	
30	10.1
40	24.0
50	6.31
60	11.3

The effect of adsorption temperature on the CO₂ adsorption was also studied for the best performing sorbent under 17% CO₂ at 3 different temperatures (e.g. 30, 40, 50 and 60 °C). The results show that total adsorption capacity increases approximately by two-fold when the temperature increases from 30 to 40 °C, however, there is a decreasing trend above 40 °C (Figure 5 and Table 4). This is different from what was observed in the literature, where the adsorption capacity decreases with the adsorption temperature. The related difference can be explained by the excessive reduction of pore size and volume of PEI-loaded sorbents and corresponding diffusion limitation. The diffusion process is accelerated with a small increase in temperature leading to higher adsorption rate while the further increase results in decrease in the adsorption capacity due to the dominating kinetic effect of the desorption process.

Conclusion

Direct air capture (DAC) is a potential method to decrease greenhouse gas emissions from both point sources and distributed sources. Solid sorbents have been considered to be more effective than liquid sorbents for DAC due to their faster kinetics and their ability to avoid volatile and heat losses caused by liquid evaporation. In this investigation, we chose alumina-supported polyethyleneimine (PEI) materials as solid sorbents and examined their CO₂ capturing behaviour for various PEI loadings (20, 35, 50 wt%), flow rates (15, 30, 45 L/h) and adsorption temperatures (30, 40, 50, 60 °C) and at 2 different CO₂ concentration (1% and 17%). The sorbents were prepared using a wetness impregnation technique and were characterized for their physical and chemical properties. Results show that 35% PEI loading has the best CO₂ capture capacity under 1% CO₂ flow with a capacity of 90.5 mg/g sorbent. However, at 17% CO₂ flow, 50% PEI loading was found to be the best choice with a capacity of 24 mg/g sorbent. The significant difference in the CO₂ adsorption capacity of sorbents between 2 different CO₂ concentrations is attributed to the strong diffusion limitation of sorbents caused by the dramatic decrease in their surface area and pore volume. We also found that the flow rate and adsorption temperature have a strong impact on the CO₂ capture capacity. Both have negative effects on the adsorption capacity. One exception was found at 40 °C, where the adsorption capacity is lower than that observed at 30C. This is also related to diffusion limited adsorption process. The relatively low solvent/PEI ratio and insufficient mixing time results in uneven distribution of PEI on alumina and a high degree of reduction in the surface area and pore volume of sorbent, which leads to the relatively low adsorption capacity due to high diffusion limitation. This issue needs to be solved for further studies.

Scientific Ethics Declaration

The authors declare that the scientific ethical and legal responsibility of this article published in EPSTEM journal belongs to the authors.

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